

Digital Filter Types in Delta-Sigma ADCs

Brian Pisani

ABSTRACT

This application report discusses digital filters which are a ubiquitous feature in delta-sigma analog to digital converters (ADCs). Digital low-pass filters are essential to the functionality of a delta-sigma ADC, which relies on oversampling and noise shaping to push quantization noise out of band. There are variations between the types of digital filters used in delta-sigma ADCs that provide various benefits and drawbacks that orient them to different applications. The types of filters and the tradeoffs between them are discussed in this report.

Contents

1	Introduction	1
2	Digital Filters in Delta-Sigma ADCs	2
3	Sinc Filter	3
4	Wideband Filters	5
5	References	7

List of Figures

1	Spectrum of Delta-Sigma Quantization Noise and a Sinc Low-Pass Filter	2
2	Wideband Filter Frequency Response.....	2
3	Sinc ³ Frequency Response.....	2
4	Frequency Response of Sinc ¹ , Sinc ³ , and Sinc ⁵ Digital Filters	4
5	Step Response for Sinc ¹ , Sinc ³ , and Sinc ⁵ Digital Filters	4
6	Magnitude Response of the ADS124S08 Digital Filter, $f_{DR} = 20$ SPS	5
7	Magnitude Response for the ADS127L01 Wideband Filter up to f_{DR}	6
8	Response of the ADS127L01 Wideband Filter to a Unit-Step Input	7

List of Tables

Trademarks

All trademarks are the property of their respective owners.

1 Introduction

Delta-sigma analog-to-digital converters (ADCs) are different from other types of data converters in that they typically integrate digital filters. The digital filter is crucial to how delta-sigma ADCs are able to obtain fine resolution across a variety of bandwidths. This application report discusses the motivation for including a digital filter in delta-sigma ADCs, the different types of digital filters, and the tradeoffs that exist between the various types of digital filters as they relate to different applications.

2 Digital Filters in Delta-Sigma ADCs

To understand why the digital filter is an important aspect in delta-sigma analog-to-digital conversion, it is critical to have a basic understanding of a delta-sigma modulator. The modulator takes its input from a sample-and-hold circuit which will sample the ADC input at a rate (f_{MOD}) many times faster than the ADC output data rate (f_{DR}).

The modulator consists of at least one integrator and a low-resolution ADC which quantizes the integrator output voltage into just a few bits. The modulator converts the result of the low-resolution ADC back to analog and feeds it back to the modulator input where it is subtracted from the input voltage as a means of error correction. The result is a discrete-time feedback system which allows sampled input signals to pass at unity gain, but will shape quantization noise density to be lower at low frequency and higher at high frequency.

In order to reduce higher-frequency quantization noise, the modulator output is fed to the digital low-pass filter. Subsequently, the signal of interest passes through to the output of the digital filter, while much of the higher-frequency quantization noise is filtered out.

Figure 1 shows quantization noise plotted with the response of a common type of low-pass digital filter found in delta-sigma ADCs called a sinc filter (its name stems from its $\sin(x) / x$ frequency response).

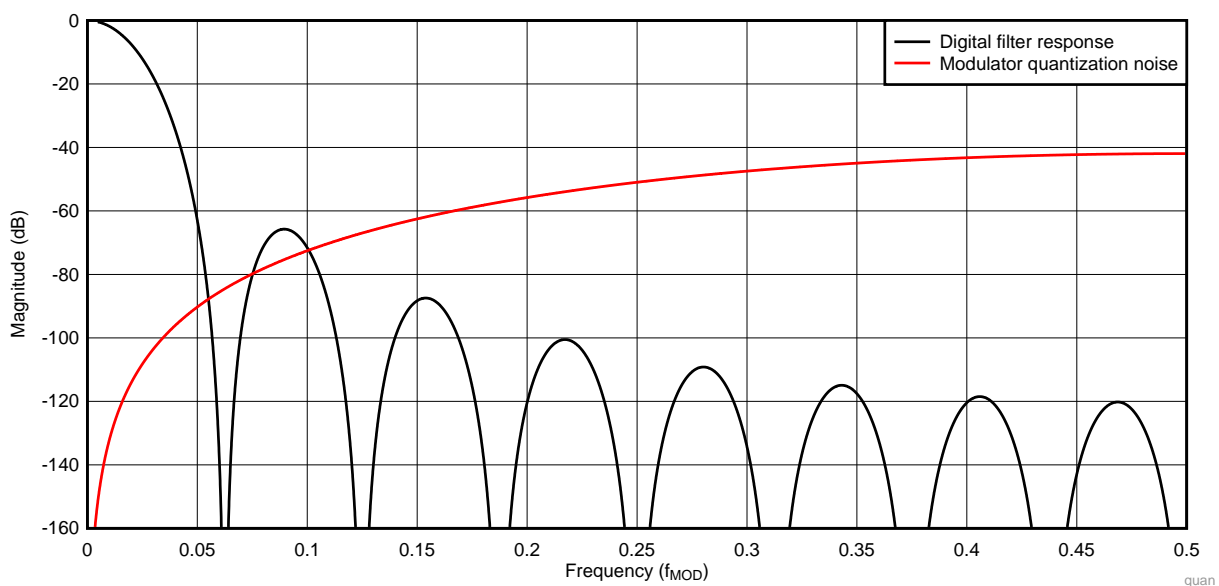
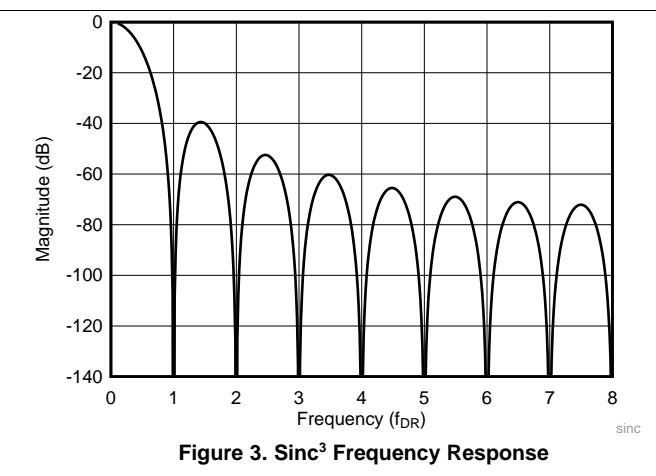
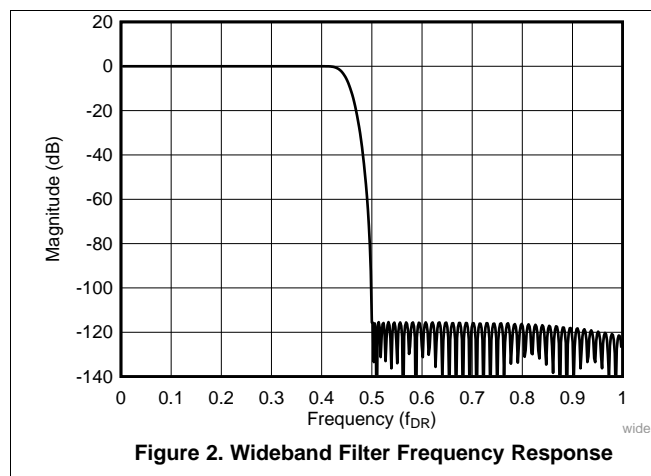


Figure 1. Spectrum of Delta-Sigma Quantization Noise and a Sinc Low-Pass Filter

Sinc filters, while extremely common, are not the only types of digital low-pass filters associated with delta-sigma ADCs. For example, some ADCs, like the ADS124S08, add an extra 50 Hz and 60 Hz notch filter designed for applications with a lot of power-line interference. On the other hand, the ADS127L01 has a wide-bandwidth flat-passband digital filter designed for higher-frequency applications.

The digital filters in delta-sigma ADCs serve another function – decimation. These filters decimate data which is output from the modulator at f_{MOD} by a factor known as the oversampling ratio (OSR). The relationship between f_{DR} and f_{MOD} is $f_{\text{DR}} = f_{\text{MOD}} / \text{OSR}$. The OSR and filter type combined determine the output bandwidth of the digital filter and overall frequency response of the ADC. Large OSRs produce small filter bandwidths, which translates to very good noise performance, simplified anti-aliasing circuitry, and reduced digital interface speeds for the host controllers.

Most digital filters in delta-sigma ADCs have a finite impulse response (FIR). These filters are inherently stable and easy to design with linear phase responses. Figure 2 and Figure 3 plot the responses of two types of FIR filters in delta-sigma ADCs side by side. Figure 2 shows the wideband filter in the ADS127L01. Figure 3 is a classic third-order sinc response filter, or sinc^3 like that found in the ADS124S08.



The benefit of using a wideband filter for AC measurement applications is clear from its magnitude response. Its nearly 0-dB gain until right before the Nyquist bandwidth of the data rate ($f_{DR} / 2$) ensures no signal power loss for frequencies in the passband. The steep transition band limits aliasing. The sinc³ filter, on the other hand, attenuates signals to -3 dB at $0.262 \times f_{DR}$ and transitions slowly even after $f_{DR} / 2$, which would enable more out-of-band noise to fold into the bandwidth of interest. Seemingly, the wideband FIR filter would be ideal for any application; however, this excellent frequency-domain performance comes at a price.

The trade-off between the wideband filter and the sinc filter is in the time domain. The wideband filter is a very high-order filter, meaning it takes a long time to settle to a final value upon receiving a step input. In the wideband filter of the ADS127L01, it will take 84 conversions to receive a settled output. A sinc³ filter settles in three conversions after a step at the input, enabling quick cycling through multiple input channels. This trade-off between frequency response and latency exists for all FIR filters.

3 Sinc Filter

The name “sinc” comes from its frequency response, which takes the form of the $\sin(x) / x$ function. The reason the filter has this response is actually tied closely with why it is so often used in delta-sigma ADCs.

The digital filter creates a digital output code by summing the modulator output over a certain number of modulator clock periods. The ratio of the modulator rate (f_{MOD}) of the delta-sigma ADC to its output data rate (f_{DR}) is the OSR. This is equivalent to taking a moving average of those samples over the sampling period. Taking the moving average in the time domain translates to a first-order sinc response in the frequency domain. The sinc response is equal to zero at integer multiples of the data rate, which appear as notches in the magnitude response plot of the filter.

The amount of averaging increases when cascading multiple sinc filters in series, thus increasing the filter order. In the spectrum, this corresponds to a lower cutoff frequency and a higher stopband attenuation, which in turn reduces noise. Figure 4 shows the difference in the frequency responses of a first-order sinc filter (sinc¹), three sinc filters in series (a third-order sinc, sinc³) and five sinc filters in series (sinc⁵).

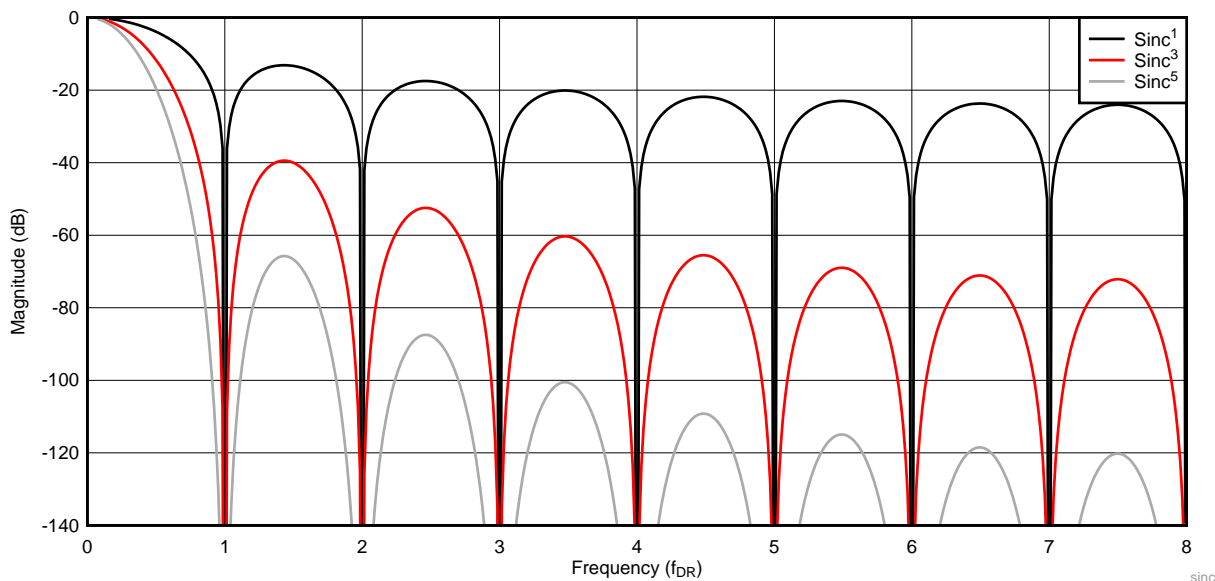


Figure 4. Frequency Response of Sinc¹, Sinc³, and Sinc⁵ Digital Filters

Looking at these responses, there does not seem to be very much bandwidth in the digital-filter output, limiting the measurable signal content. This is not a drawback in certain low-bandwidth applications. Some precision sensor applications, like temperature and pressure sensors, do not require much bandwidth for measurement, but need a good low-pass filter to reject out-of-band noise. The sinc filter fits well into these applications.

Given the application, it may be desirable to multiplex between multiple sensor inputs relatively quickly. To do this, the digital filter needs to respond to an input change and settle quickly. The sinc filter is ideal for this, too. Sinc filters offer much faster settling times relative to other digital filters with more finely tuned frequency responses. In many cases, these filters can be built to settle to a step input in a single conversion cycle.

Nevertheless, trade-offs exist even between the types of sinc filters. The higher order a sinc filter is, the longer it will take to settle – but with the bonus of better stop-band attenuation. Figure 5 shows how the sinc¹, sinc³ and sinc⁵ filters respond to a unit step input. Note that the order of the sinc filter matches the number of samples it takes to settle to the input.

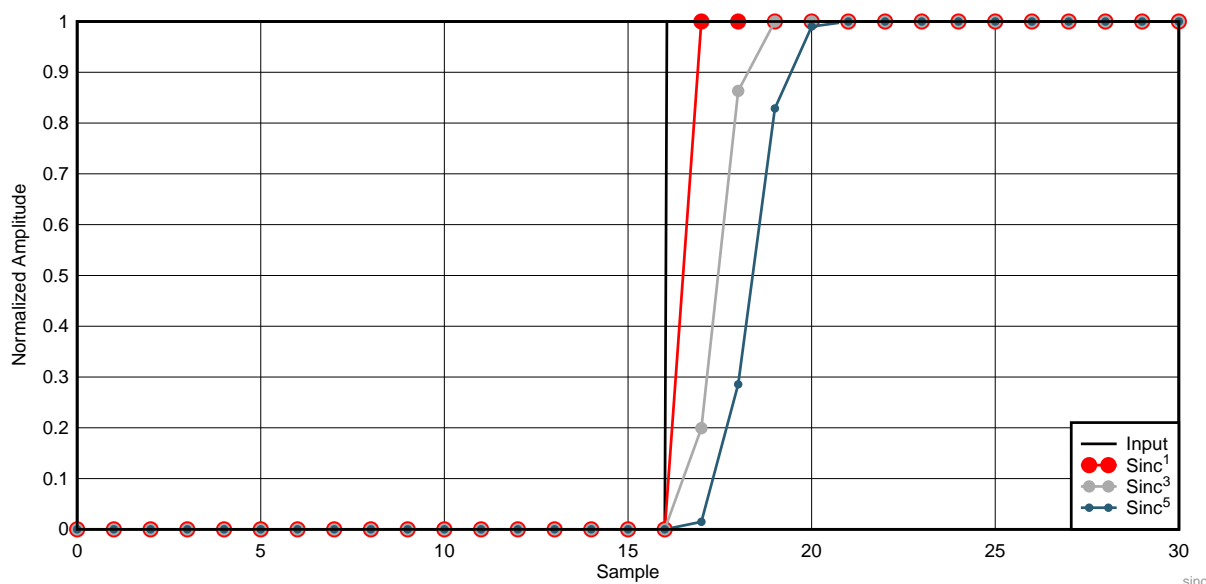


Figure 5. Step Response for Sinc¹, Sinc³, and Sinc⁵ Digital Filters

Some data converters have slightly modified sinc filters. In some industrial applications, power utility interference pollutes the environment of the equipment at 50 Hz or 60 Hz. A digital filter that has notches in its frequency response at 50 Hz or 60 Hz helps reject the utility frequency and maintain high system power-supply rejection (PSR).

In many cases, these filters can be built to settle to a step input in a single conversion cycle. However, a filter that settles within a single cycle will not have as much out-of-band rejection as an unmodified higher-order sinc filter. Figure 6 shows the magnitude response of the digital filter on the ADS124S08 when the data rate is set to 20 SPS using the low-latency filter. Note that this filter simultaneously rejects both 50 Hz and 60 Hz. A normal sinc filter would require a data rate at some integer divisor of 10 SPS to achieve this, since filter notches would occur at multiples of 10 Hz.

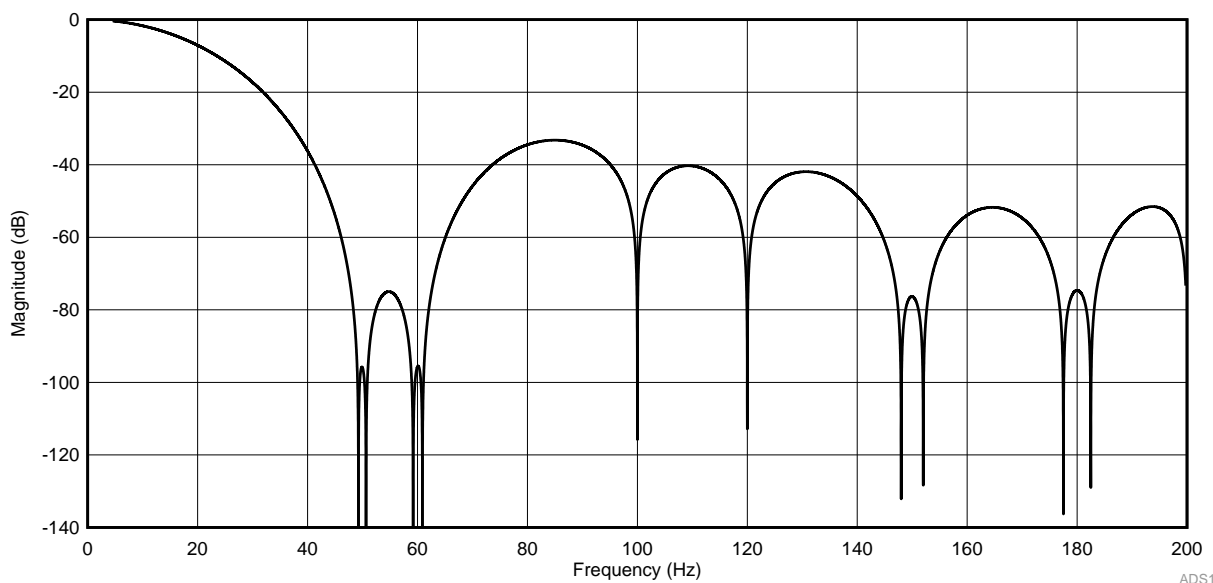


Figure 6. Magnitude Response of the ADS124S08 Digital Filter, $f_{DR} = 20$ SPS

In summary, the sinc filter is used as a basic low-pass filter in delta-sigma ADCs. Their reasonable stopband attenuation combined with their quick step response make them ideal for dc measurement applications, especially when multiplexing between several input signals.

4 Wideband Filters

Even though delta-sigma ADCs with sinc filters are a great fit for low-bandwidth applications, the delta-sigma architecture can also be used with great success in higher bandwidth applications as well. For example, precisely measuring audio or vibration signals can be done using delta-sigma ADCs. Test and measurement equipment that requires high bandwidth is another application well-suited for delta-sigma ADCs. For these applications, a wideband filter can be used as the integrated digital filter on a delta-sigma ADC.

AC applications require a wide passband with little attenuation or ripple, but still require the precision that comes standard with the oversampling topology of a delta-sigma ADC. That is why some ADCs are designed with a wide passband filter that has a steep transition band. The ADS127L01, a 24-bit delta-sigma ADC optimized for wide-bandwidth applications, has such a filter. Figure 7 shows the magnitude response of the filter up to the output data rate, f_{DR} , of the ADC, which is 512 kHz. Note how steep the transition band of the filter is around $f_{DR} / 2$ – the frequency where signals begin to alias into the passband. This serves to drastically limit unwanted signals or noise from folding over. The stopband magnitude never exceeds –116 dB until the response of the filter repeats around the modulator frequency, f_{MOD} , of the ADC.

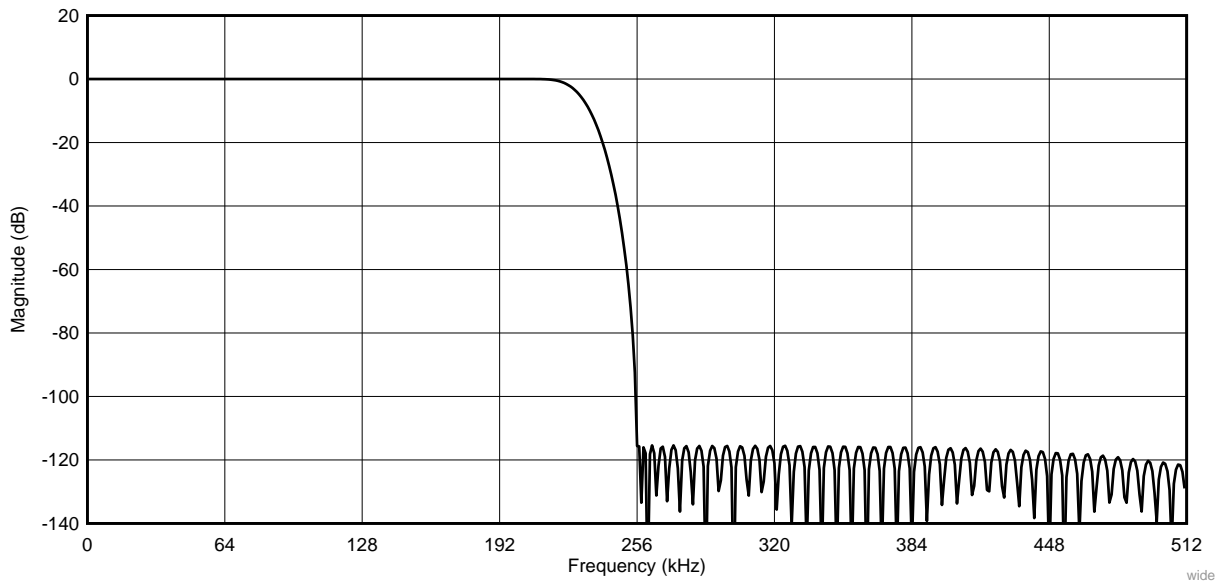


Figure 7. Magnitude Response for the ADS127L01 Wideband Filter up to f_{DR}

For higher-bandwidth applications, the sinc filter is less adequate for a few reasons. First, the frequency response rolls off early and droops at relatively low frequencies. This limits the usable signal bandwidth. On the other hand, the wideband filter remains almost perfectly flat until around $f_{DR} / 2$, maximizing the usable signal bandwidth for any given data rate.

Second, aliasing is more of a concern for AC applications. The sinc filter is not ideal because it does not attenuate sufficiently at half the output data rate, $f_{DR} / 2$, of the ADC. Alternatively, the wideband filter features exceptional stopband attenuation, which minimizes aliasing.

For ADCs without integrated digital filters, options are limited for achieving such a steep anti-aliasing response. High-order analog anti-aliasing filters with steep roll-offs are notoriously difficult to design and are subject to component tolerances and temperature. Alternatively, it is possible to oversample the converter and digitally filter in the processor, but this comes at the cost of instruction cycles, which may be scarce in high-speed applications. A wideband filter in a delta-sigma ADC truly solves this problem with its built-in “oversample, low-pass filter, then decimate” topology.

There is a trade-off with all digital filters where superb frequency-domain performance is achieved in exchange for longer settling times. After applying a step function to the input, the digital filter of the ADS127L01 requires 84 output sample periods to settle to the final output. For this reason, wideband filters are not ideal for applications that cycle between multiple-signal source inputs.

Figure 8 shows the step response of the wideband filter of the ADS127L01.

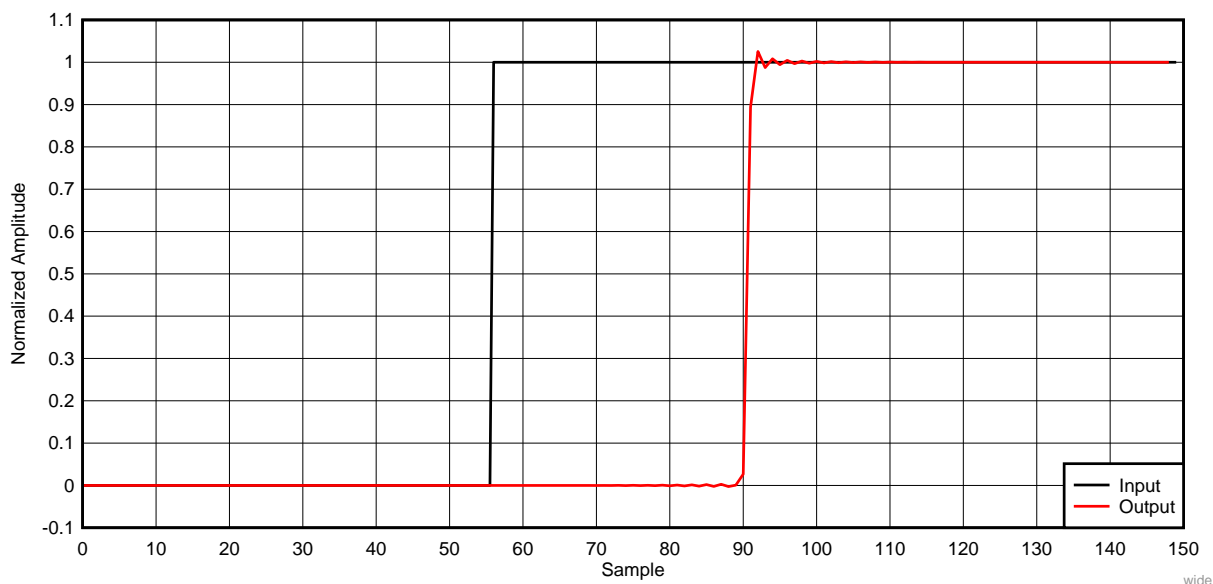


Figure 8. Response of the ADS127L01 Wideband Filter to a Unit-Step Input

The filter has a linear phase response, which means that its group delay (the delay due to phase shifting) will be constant across frequencies. For this filter, the group delay is 42 output data samples.

The wideband digital filter in delta-sigma ADCs provides an ideal functional block for wide-bandwidth, precision-measurement signal chains where no multiplexing between different signal sources is required. The flat passband with low ripple ensures that no in-band signal content is lost, and the steep transition and excellent stopband attenuation provide flexibility in environments where anti-aliasing is critical. In addition, the precision expected from a delta-sigma ADC can still be enjoyed.

5 References

- [ADS124S08](#) data sheet (SBAS660)
- [ADS127L01](#) data sheet (SBAS607)

IMPORTANT NOTICE FOR TI DESIGN INFORMATION AND RESOURCES

Texas Instruments Incorporated ("TI") technical, application or other design advice, services or information, including, but not limited to, reference designs and materials relating to evaluation modules, (collectively, "TI Resources") are intended to assist designers who are developing applications that incorporate TI products; by downloading, accessing or using any particular TI Resource in any way, you (individually or, if you are acting on behalf of a company, your company) agree to use it solely for this purpose and subject to the terms of this Notice.

TI's provision of TI Resources does not expand or otherwise alter TI's applicable published warranties or warranty disclaimers for TI products, and no additional obligations or liabilities arise from TI providing such TI Resources. TI reserves the right to make corrections, enhancements, improvements and other changes to its TI Resources.

You understand and agree that you remain responsible for using your independent analysis, evaluation and judgment in designing your applications and that you have full and exclusive responsibility to assure the safety of your applications and compliance of your applications (and of all TI products used in or for your applications) with all applicable regulations, laws and other applicable requirements. You represent that, with respect to your applications, you have all the necessary expertise to create and implement safeguards that (1) anticipate dangerous consequences of failures, (2) monitor failures and their consequences, and (3) lessen the likelihood of failures that might cause harm and take appropriate actions. You agree that prior to using or distributing any applications that include TI products, you will thoroughly test such applications and the functionality of such TI products as used in such applications. TI has not conducted any testing other than that specifically described in the published documentation for a particular TI Resource.

You are authorized to use, copy and modify any individual TI Resource only in connection with the development of applications that include the TI product(s) identified in such TI Resource. NO OTHER LICENSE, EXPRESS OR IMPLIED, BY ESTOPPEL OR OTHERWISE TO ANY OTHER TI INTELLECTUAL PROPERTY RIGHT, AND NO LICENSE TO ANY TECHNOLOGY OR INTELLECTUAL PROPERTY RIGHT OF TI OR ANY THIRD PARTY IS GRANTED HEREIN, including but not limited to any patent right, copyright, mask work right, or other intellectual property right relating to any combination, machine, or process in which TI products or services are used. Information regarding or referencing third-party products or services does not constitute a license to use such products or services, or a warranty or endorsement thereof. Use of TI Resources may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

TI RESOURCES ARE PROVIDED "AS IS" AND WITH ALL FAULTS. TI DISCLAIMS ALL OTHER WARRANTIES OR REPRESENTATIONS, EXPRESS OR IMPLIED, REGARDING TI RESOURCES OR USE THEREOF, INCLUDING BUT NOT LIMITED TO ACCURACY OR COMPLETENESS, TITLE, ANY EPIDEMIC FAILURE WARRANTY AND ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE, AND NON-INFRINGEMENT OF ANY THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

TI SHALL NOT BE LIABLE FOR AND SHALL NOT DEFEND OR INDEMNIFY YOU AGAINST ANY CLAIM, INCLUDING BUT NOT LIMITED TO ANY INFRINGEMENT CLAIM THAT RELATES TO OR IS BASED ON ANY COMBINATION OF PRODUCTS EVEN IF DESCRIBED IN TI RESOURCES OR OTHERWISE. IN NO EVENT SHALL TI BE LIABLE FOR ANY ACTUAL, DIRECT, SPECIAL, COLLATERAL, INDIRECT, PUNITIVE, INCIDENTAL, CONSEQUENTIAL OR EXEMPLARY DAMAGES IN CONNECTION WITH OR ARISING OUT OF TI RESOURCES OR USE THEREOF, AND REGARDLESS OF WHETHER TI HAS BEEN ADVISED OF THE POSSIBILITY OF SUCH DAMAGES.

You agree to fully indemnify TI and its representatives against any damages, costs, losses, and/or liabilities arising out of your non-compliance with the terms and provisions of this Notice.

This Notice applies to TI Resources. Additional terms apply to the use and purchase of certain types of materials, TI products and services. These include; without limitation, TI's standard terms for semiconductor products (<http://www.ti.com/sc/docs/stdterms.htm>), [evaluation modules](#), and [samples](http://www.ti.com/sc/docs/sampterm.htm) (<http://www.ti.com/sc/docs/sampterm.htm>).

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265
Copyright © 2017, Texas Instruments Incorporated